

SUPPLEMENTAL STRUCTURAL CALCULATIONS

PIN PILE FOUNDATION

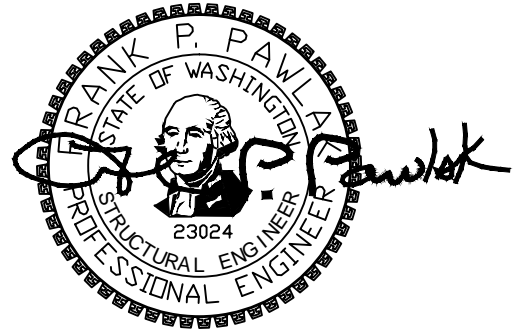
9820 SE 35th Place Remodel

Mercer Island, Washington

PROJECT NO.: 20-129

DATE: FEBRUARY 16, 2022

02/16/2022



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9820 SE 35th PI

Pin Pile Foundation Revision

The condition of site soils has necessitated the use of pin piles to support the new structure. The geotechnical engineer has confirmed. 2" dia driven pipe piles will be used with a 3T capacity. The floor slab will be soil supported.

Reposition Shear Wall at Fireplace

The SW-3 shear wall adjacent to the fireplace has been moved to the end wall over the C15 channel. The attached calc checks the channel and outrigger for max loading and omega seismic forces. The framing is found to be adequate.



9820 SE 35th PI

SUBJECT

PROJECT

CLIENT

FPP
DESIGN

20-129

PROJECT NO.

2/22

DATE

1

SHEET NO.

EAST WALL ON GRID 'A': LOAD BEARING WALL

$$DL = 25 \text{ PSF} (7.75') + 8 (12 \text{ PSF}) = 290 \text{ P/F}$$

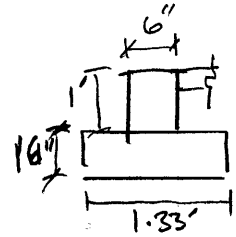
$$LL = 60 \text{ PSF} (7.75') = 465 \text{ P/F}$$

$$W_G = DL + LL = 755 \text{ P/F}$$

$$W_{FTG} = 150 \text{ PCF} \times 1.33' \times \frac{16'}{12} = 266 \text{ P/F}$$

$$W_{STEM} = 150 \text{ PCF} \times 1' \times 6\frac{1}{2}' = \underline{75 \text{ P/F}}$$

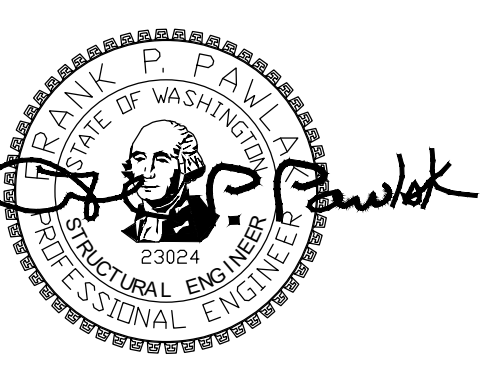
$$\Sigma W = \underline{1096 \text{ P/F}}$$



NON-LOAD BEARING WALL:

$$\Sigma W = 266 + 75 = 341 \text{ P/F}$$

$$\text{PILE SPACING} = \frac{6000}{341} = \underline{17} \text{ o.c. max}$$



PROJECT

9820 SE 35TH PLACE
 ACHIN & MARY CHEN
 9820 SE 35TH PL
 MERCER ISLAND, WA 98040

REVISIONS

NO.	DATE	DESCRIPTION
11-4-20	PERMIT	
4/2/21	PERMIT RESPONSE	
1/26/22	REVISIONS	

11/4/20	20-129
DATE	JOB #
AM	FPP
DESIGN	CHECKED
LMS	AS NOTED
DRAWN	SCALE

SDCI STAMP

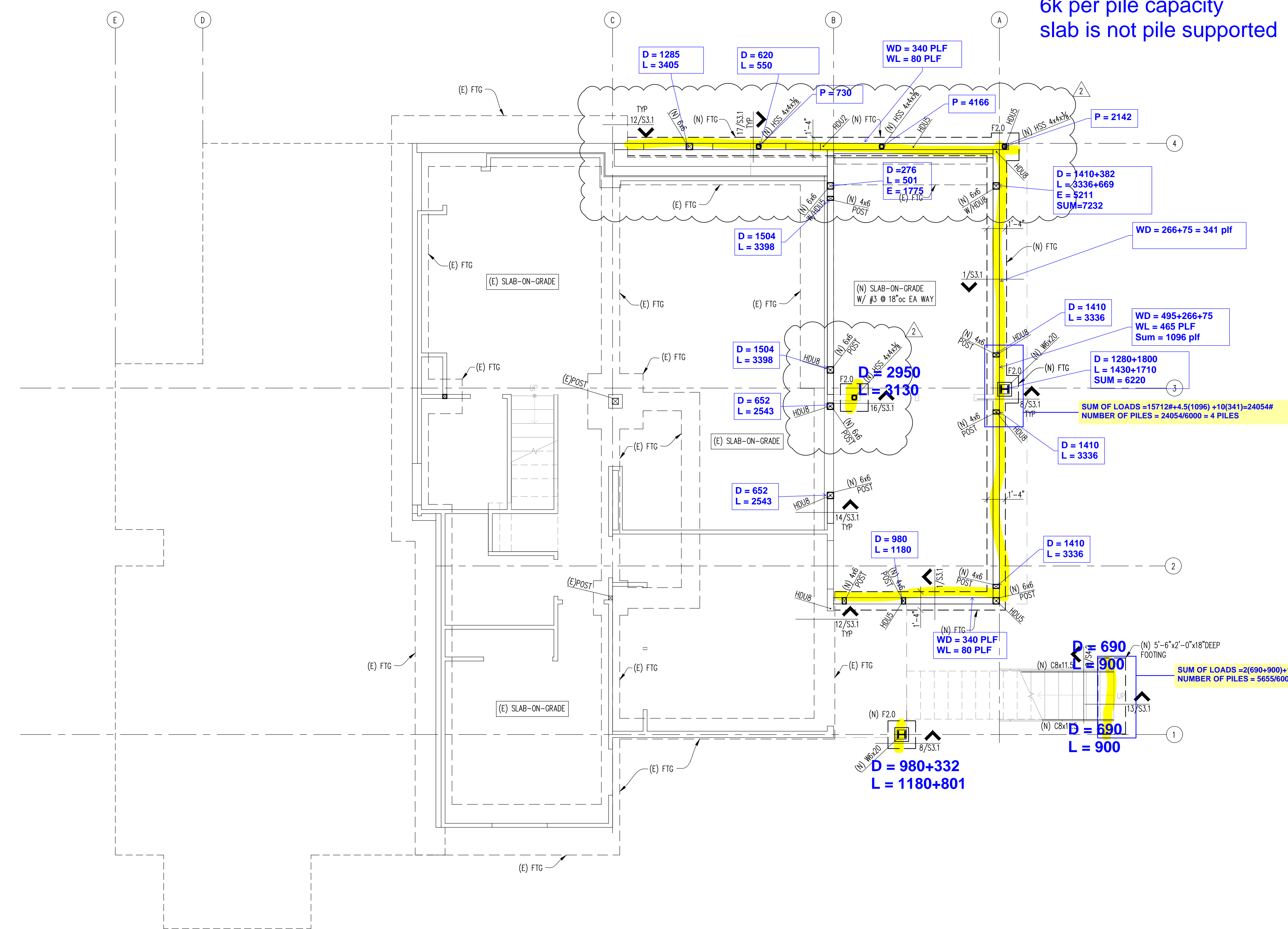
SHEET TITLE

FOUNDATION PLAN

SHEET NO.

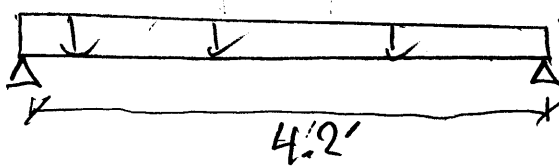
S2.1

pin pile foundation
 2" dia pipe
 6k per pile capacity
 slab is not pile supported



GRADE BEAM @ GRID A 3 3

WORST CASE



$$\begin{aligned} \Sigma W_u &= 1.2(290 + 266 + 75) \\ &+ 1.6(465) = 1502 \text{ PLF} \end{aligned}$$

$$M_u = \frac{wL^2}{8} = \frac{1502(4.2)^2}{8} = \underline{3.8} \text{ k-ft}$$

$$V_u = \frac{wL}{2} = \frac{1502(4.2)}{2} = \underline{3.2} \text{ k}$$

(2) #5 cont T&B

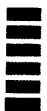
$$A_s = .62 \text{ in}^2$$

$$b = 16''$$

$$d = 12.5''$$

$$\phi M_n = 33.3 \text{ k-ft OK}$$

$$v_u = 3.2 / (.75 * 16 * 12.5) = .021 \text{ ksi USE \#4 @ 12 stirrups}$$



FOSSATTI PAWLAK
STRUCTURAL ENGINEERS

9820 SE 35th PI

PROJECT

SUBJECT

PROJECT NO.

DATE

MT

DESIGN

SHEET NO.

Check CIS + OUTRIGGER TO SUPPORT SW

$V_s = 2.365^k$ service

$P = \pm 3423^{\#}$

$\omega_c = 2.5$

$P_s = \frac{2.365(\frac{1}{2})(9.25)}{1.3} \times 2.5 = \pm 7.65^k$

$m = 1.76(14.92) - 0.65(14.92)^2/2$
 $= 19^k$

CIS OK

SEE OUTPUT

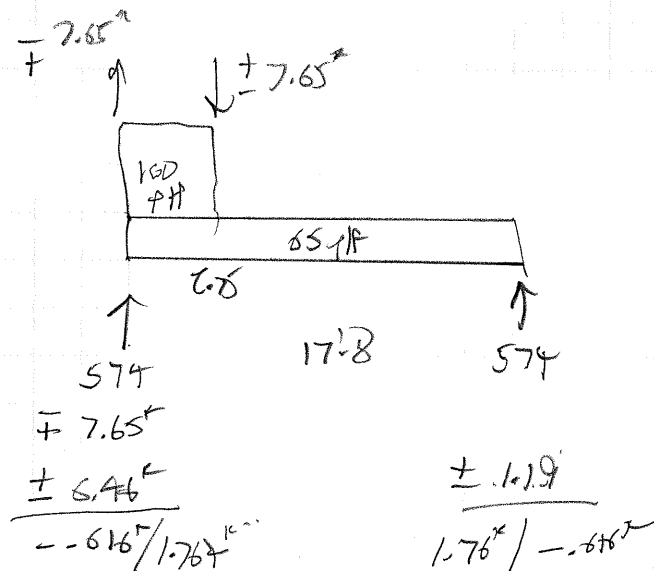
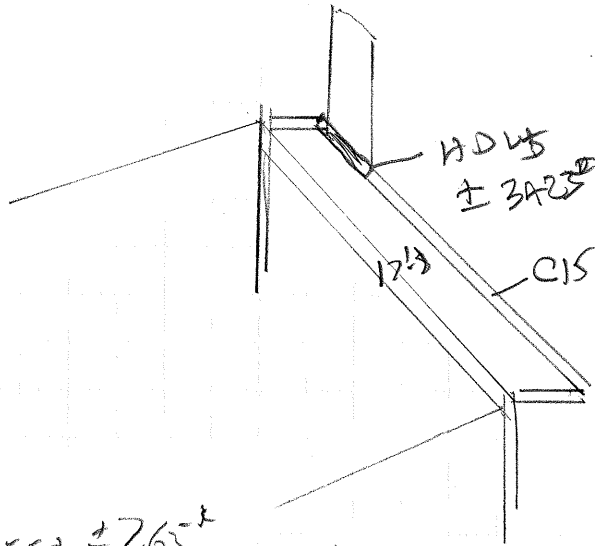
Check OUTRIGGER

$M = 574(20) + (3423 - 2870)(20) = 22,134^{11-k}$

HSS 5x4x1/2 $S_x = 8.49 \text{ in}^2$

$f_y = 206 \text{ ksi}$ ✓

$\Delta = .005^{\#}$ ✓





Gravity Beam Design

STEEL CODE: AISC 360-05 ASD

SPAN INFORMATION (ft): I-End (0.00,0.00) J-End (17.67,0.00)

Beam Size (User Selected) = C15X33.9 Fy = 36.0 ksi
 Total Beam Length (ft) = 17.67
 Mp (kip-ft) = 152.40
 Top flange not braced by decking.

POINT LOADS (kips):

Dist (ft)	DL	LL	Flange Bracing	
			Top	Bottom
2.750	0.00	7.65	No	No

LINE LOADS (k/ft):

Load	Dist (ft)	DL	LL
1	0.000	0.034	0.000
	17.670	0.034	0.000
2	0.000	0.030	0.000
	17.670	0.030	0.000

no LOADS
C15 OK!

SHEAR: Max Va (DL+LL) = 7.03 kips Vn/1.67 = 77.60 kips

MOMENTS:

Span	Cond	LoadCombo	Ma kip-ft	@ ft	Lb ft	Cb	Ω	Mn / Ω kip-ft
Center	Max +	DL+LL	19.1	2.8	17.7	1.37	1.67	57.02
Controlling		DL+LL	19.1	2.8	17.7	1.37	1.67	57.02

REACTIONS (kips):

	Left	Right
DL reaction	0.57	0.57
Max +LL reaction	6.46	1.19
Max +total reaction	7.03	1.76

DEFLECTIONS:

Dead load (in)	at	8.83 ft =	-0.015	L/D =	13792
Live load (in)	at	7.77 ft =	-0.077	L/D =	2761
Net Total load (in)	at	7.77 ft =	-0.092	L/D =	2307